

0.5A,100V High Efficiency Synchronous Step-Down DC/DC Converter

General Description

AS2461 is a high efficiency monolithic synchronous step-down DC/DC converter utilizing a constant frequency, average current mode control architecture. Capable of delivering up to 0.5A continuous load with excellent line regulation. The device operates from an input voltage range of 7.5V to 100V and provides an adjustable output voltage from 1.0V to 60V.

The AS2461 features short circuit and thermal protection circuits to increase system reliability. The internal soft-start avoids input inrush current during startup.

The AS2461 require a minimum number of external components and a wide array of protection features to enhance reliability.

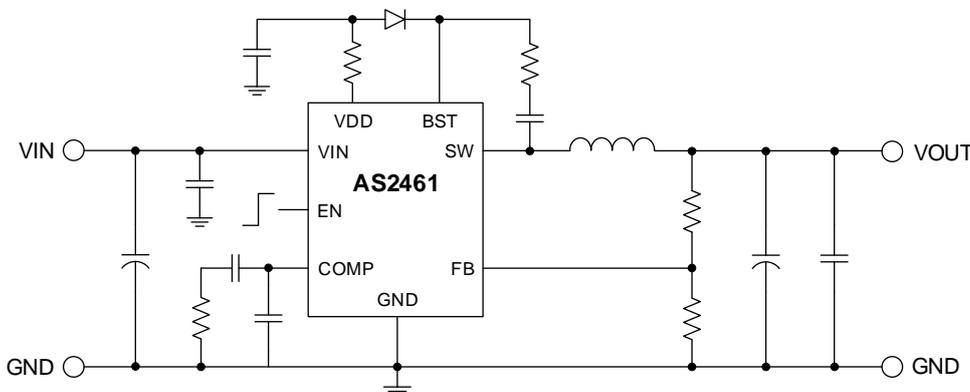
Features

- VIN Range: 7.5V to 100V
- 0.5A Continuous Output Current
- 350 μ A Quiescent Current
- Adjustable Output Voltages
- Output Voltage Accuracy : $\pm 2\%$
- Integrated 300m Ω High Side Switch
- Integrated 300m Ω Low Side Switch
- Frequency: 350kHz
- Burst Mode Operation at Light Load
- Cycle-by-Cycle Over Current Protection
- Output Short Circuit Protection with Hiccup
- Internal Soft Start
- Available in SOP8 Package

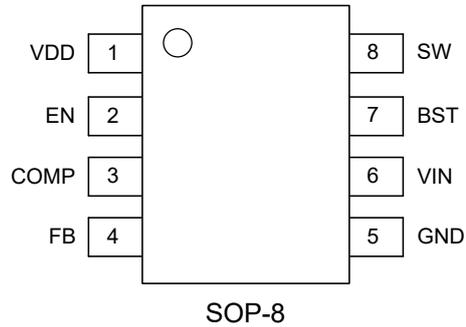
Applications

- High Voltage Power Conversion
- Automotive Systems
- Distributed Power Systems
- Battery Powered Systems
- Industrial Power Systems

Typical Applications



Pin Configuration



Pin Descriptions

PIN No.	Name	Description
1	VDD	Output of the Internal Bias Regulator
2	EN	Enable Input. Active High or Floating
3	COMP	Compensation. The Output of Internal Error Amplifier
4	FB	Feedback. Connect an External Resistive Divider to Set the Output Voltage
5	GND	Ground
6	VIN	Power Input
7	BST	Bootstrap
8	SW	Switching, Connected with a Inductor

Ordering Information

Product model	Packaging form	Smallest packaging	Logo
AS2461	SOP-8	4000PCS	AS2461

Absolute Maximum Ratings

(at $T_A = 25^\circ\text{C}$)

Characteristics	Symbol	Rating	Unit
VIN to GND		-0.3 to 105	V
SW to GND		-0.3 to VIN+0.3	V
BST to SW		-0.3 to 6.5	V
All other Pins		-0.3 to 6.5	V
Operating Junction Temperature	T_A	-40 to 150	$^\circ\text{C}$
Storage Junction Temperature	T_{stg}	-65 to 150	$^\circ\text{C}$

Notes:

Stresses at or above those listed under Absolute Maximum Ratings may cause permanent damage to the product. This is a stress rating only; functional operation of the product at these or any other conditions above those indicated in the operational section of this specification is not implied. Operation beyond the maximum operating conditions for extended periods may affect product reliability.

Recommended Operating Range

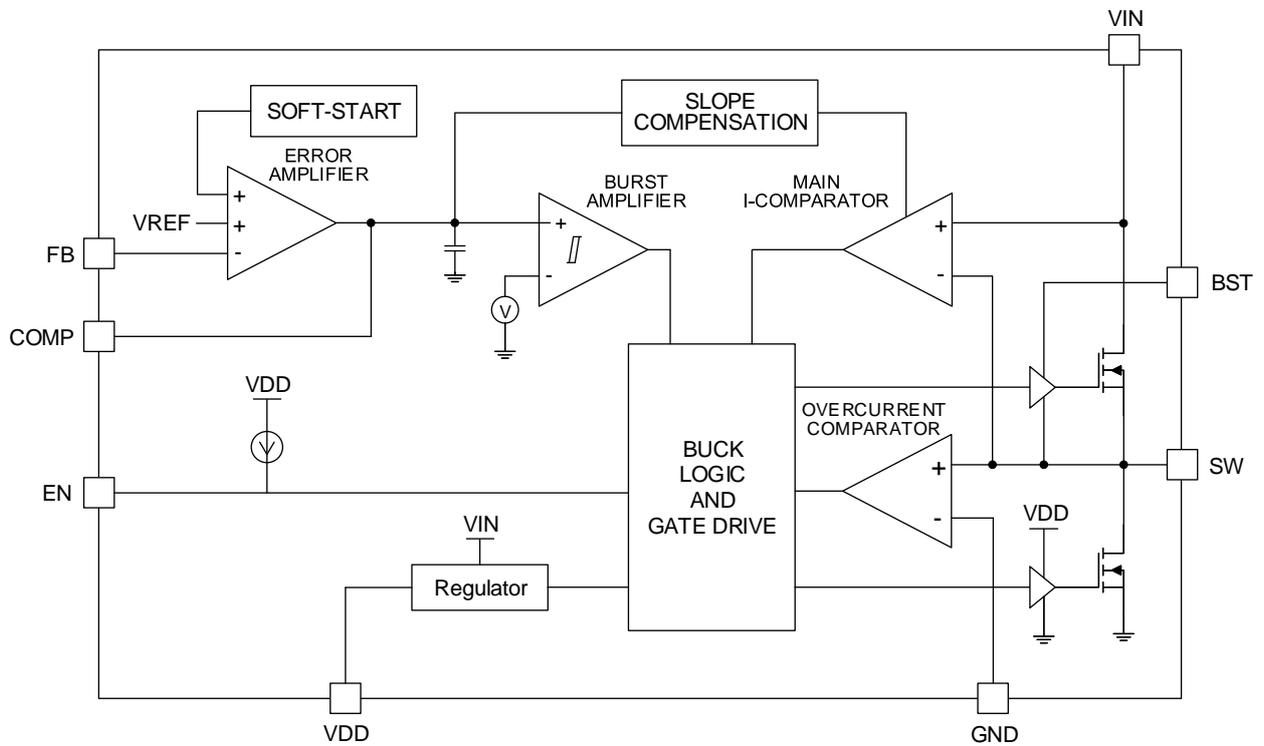
Electrical Parameter	Minimum	Typical	Maximum	Unit
Input Voltage (V_{IN})	8		80	V
Output Voltage (V_{OUT})	3.3		36	V
Output Current (I_{OUT})			0.5	A
Thermal Resistance from Junction to case (θ_{JC})		45		$^\circ\text{C}/\text{W}$
Thermal Resistance from Junction to ambient (θ_{JA})		90		$^\circ\text{C}/\text{W}$

Electrical Characteristics

($T_J = 25^\circ\text{C}$, $V_{IN} = 12\text{V}$, unless otherwise noted)

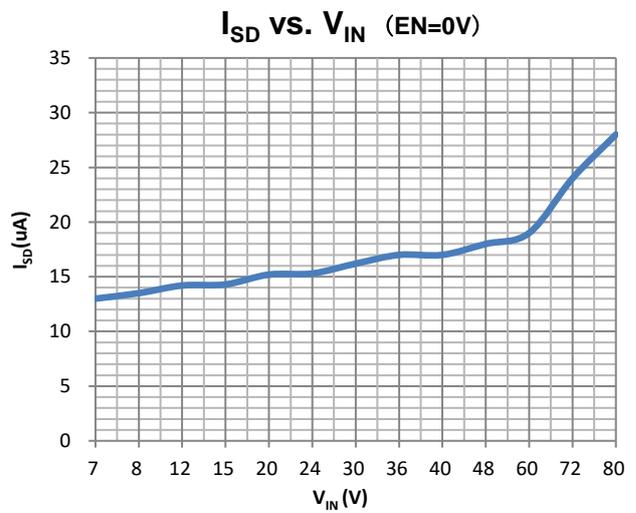
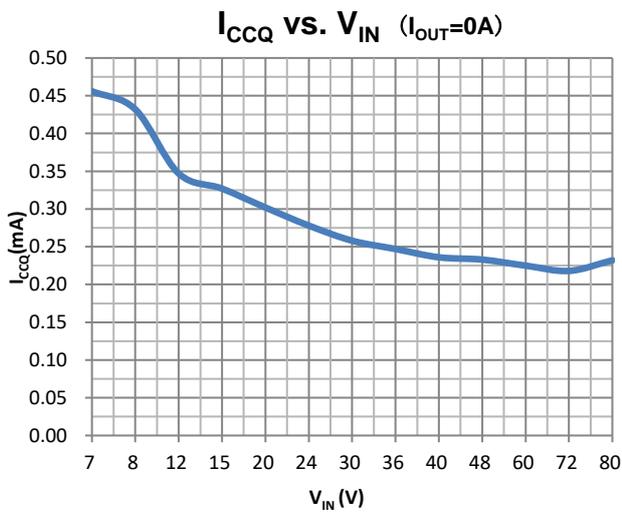
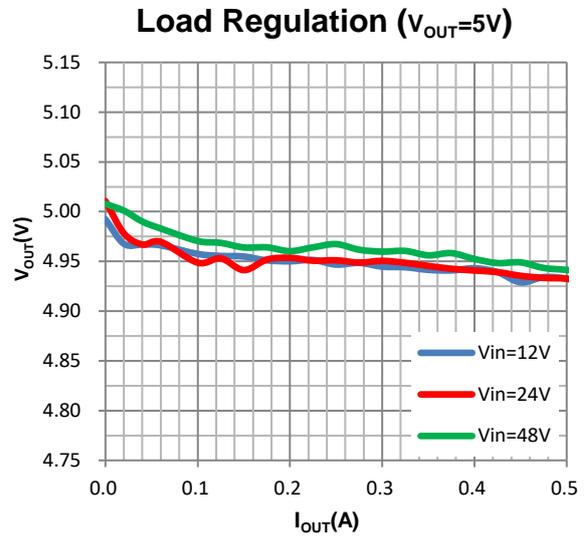
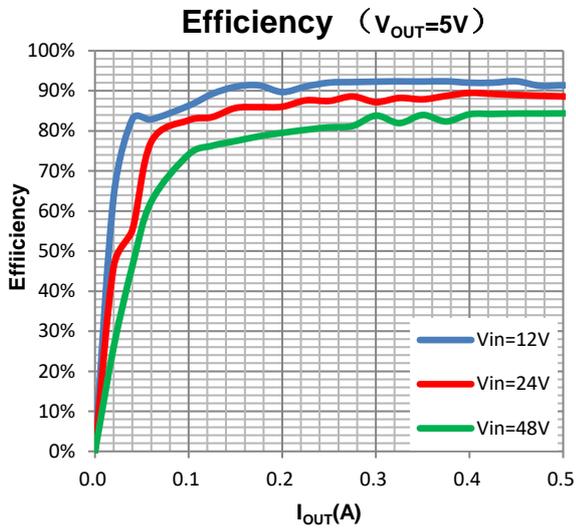
Characteristics	Symbol	Conditions	Min	Typ	Max	Units
Input Voltage	V_{IN}		7.5	-	100	V
UVLO OFF Voltage	V_{UVLO_OFF}	V_{IN} Rising		4.7	5	V
UVLO ON Voltage	V_{UVLO_ON}	V_{IN} Falling	4	4.4		V
Quiescent Current	I_{CCQ}	No Load		350		μA
Shut Down Current	I_{SD}	EN=0V		15	30	μA
FB Reference Voltage	V_{REF}		0.98	1	1.02	V
Switching Frequency	F_{SW}		320	350	380	kHz
Enable ON Voltage	V_{EN_H}	V_{EN} Rising		0.77	1	V
Enable OFF Voltage	V_{EN_L}	V_{EN} Falling	0.1	0.3		V
Maximum Duty Cycle				98		%
Minimum On-Time				100		ns
Current Limit	I_{LIMIT}		1			A
V_{FB} Short Protect	V_{FBSCP}			60		%
Hiccup Interval	T_{HICCUP}			450		ms
Soft Start Time	T_{SS}			1.3		ms
$R_{DS(on)}$ of Power MOSFET	$R_{DS(on)_H}$	Temperature=25°C		300		m Ω
	$R_{DS(on)_L}$	Temperature=25°C		300		m Ω
Thermal shutdown Temperature	T_{SD}			155		°C
Thermal Shutdown Hysteresis Temperature	T_{SH}			30		°C

Block Diagram



Typical Performance Characteristics

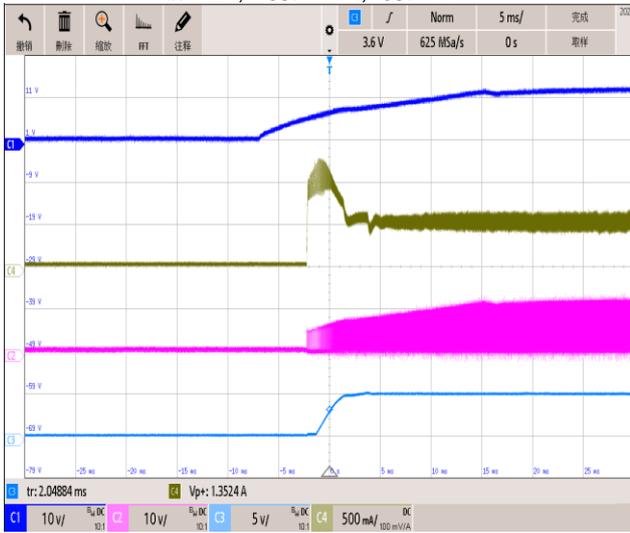
(T_J = 25°C, V_{IN} = 12V, unless otherwise noted)



CH1=V_{IN}, CH2=V_{SW}, CH3=V_{OUT}, CH4=I_{SW}, unless otherwise noted.

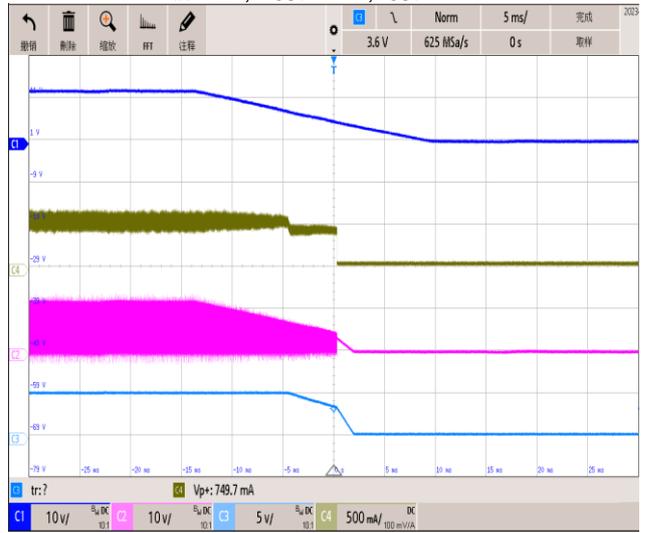
Power ON

V_{IN}=12V, V_{OUT}=5.0V, I_{OUT}=0.5A



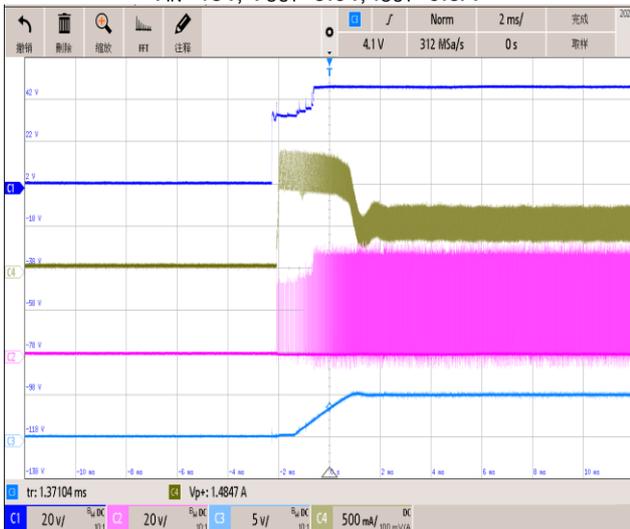
Power OFF

V_{IN}=12V, V_{OUT}=5.0V, I_{OUT}=0.5A



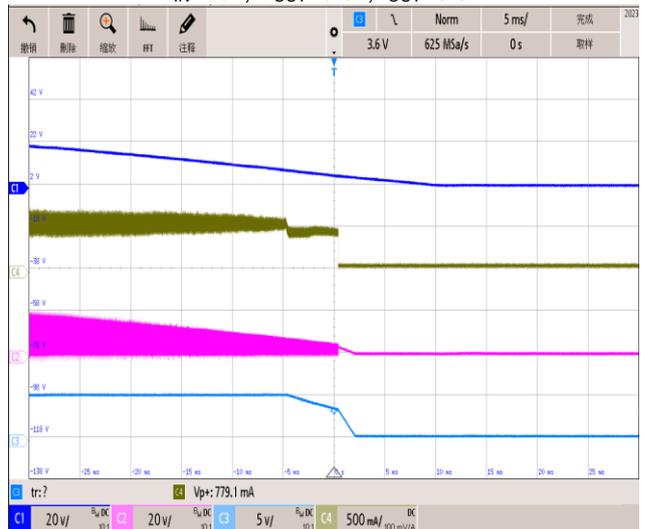
Power ON

V_{IN}=48V, V_{OUT}=5.0V, I_{OUT}=0.5A



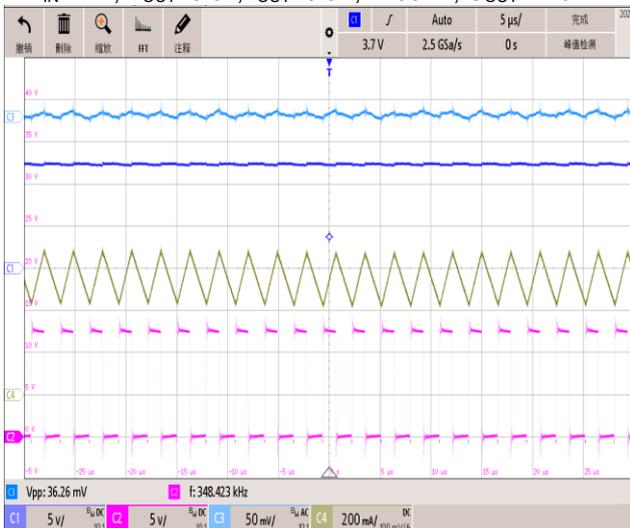
Power OFF

V_{IN}=48V, V_{OUT}=5.0V, I_{OUT}=0.5A



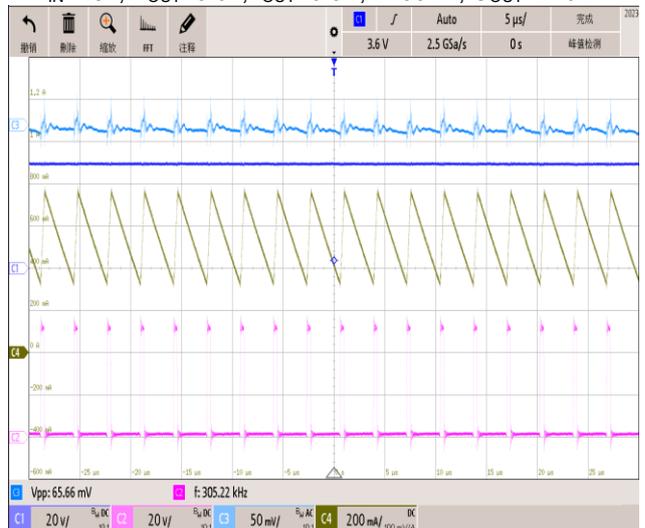
Output Voltage Ripple

V_{IN}=12V, V_{OUT}=5.0V, I_{OUT}=0.5A, L=33uH, C_{OUT}=270uF



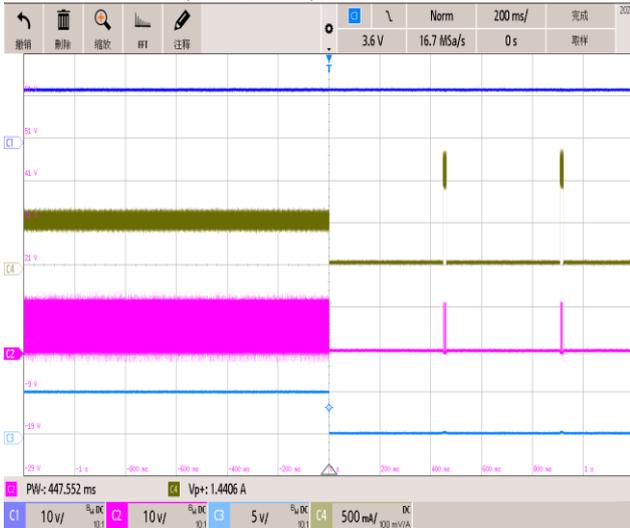
Output Voltage Ripple

V_{IN}=48V, V_{OUT}=5.0V, I_{OUT}=0.5A, L=33uH, C_{OUT}=270uF



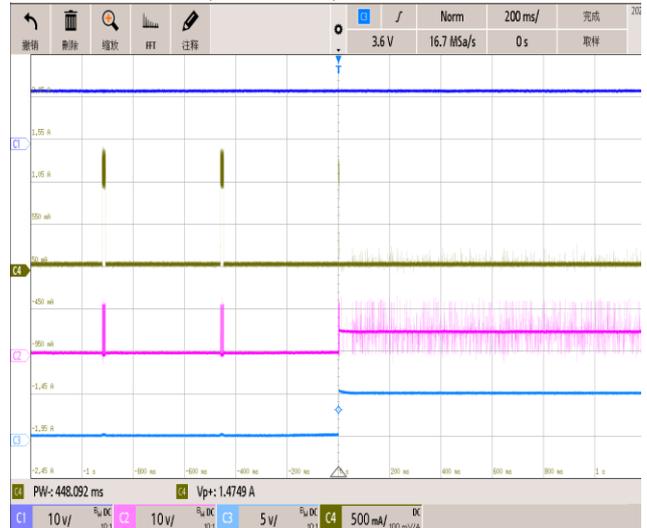
Short Circuit

$V_{IN}=12V, V_{OUT}=5.0V, I_{OUT}=0.5A$ to Short



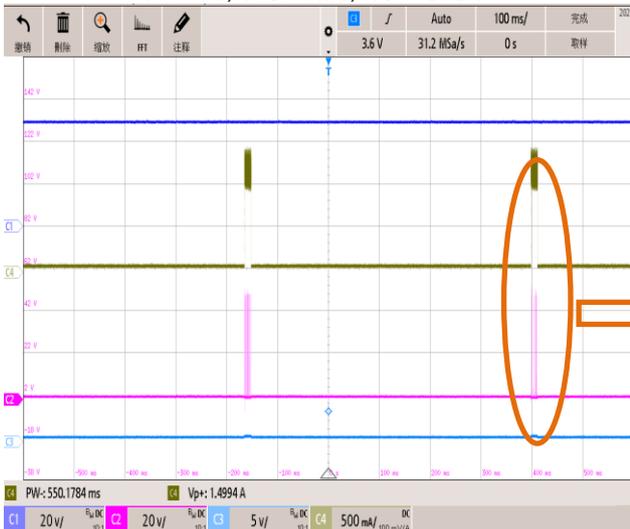
Short Circuit

$V_{IN}=12V, V_{OUT}=5.0V, I_{OUT}=$ Short to 0A



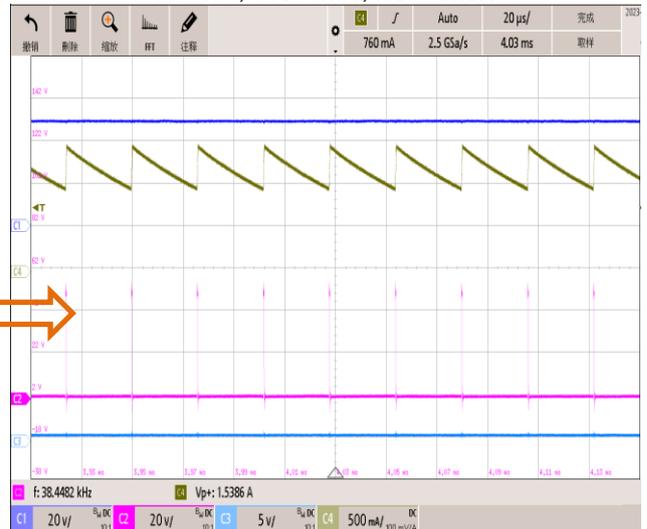
Short Circuit

$V_{IN}=48V, V_{OUT}=5.0V, I_{OUT}=$ Short



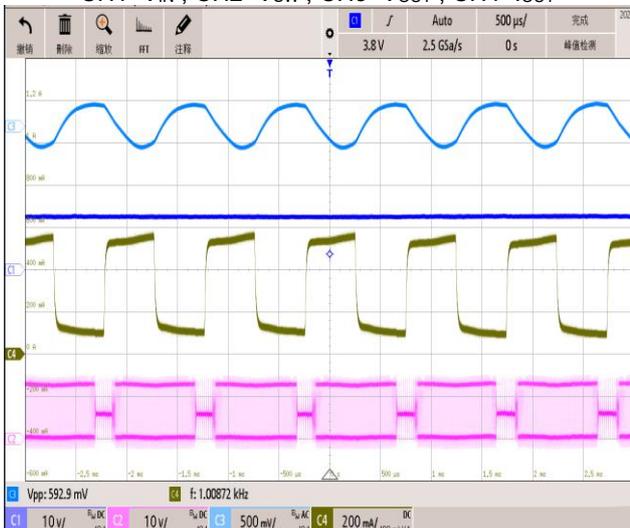
Short Circuit

$V_{IN}=48V, V_{OUT}=5.0V, I_{OUT}=$ Short



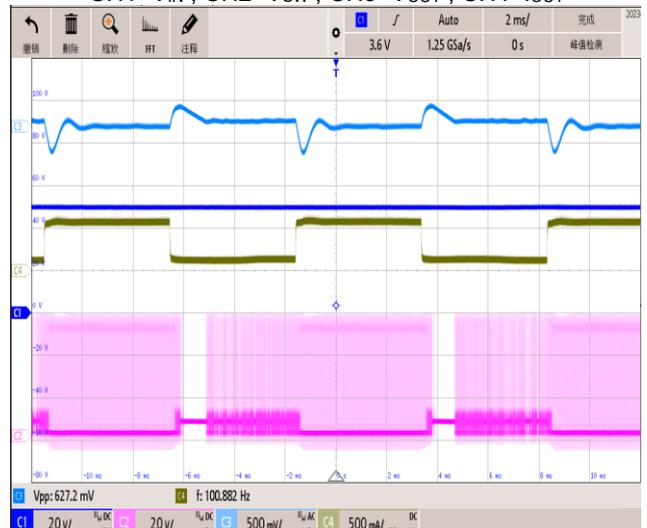
Load Dynamic Response

$V_{IN}=12V, V_{OUT}=5.0V, I_{OUT}=0.05A$ to $0.5A$,
Frequency=1kHz, Duty=50%, $C_{IN}=100\mu F, C_{OUT}=270\mu F$
CH1= V_{IN} , CH2= V_{SW} , CH3= V_{OUT} , CH4= I_{OUT}



Load Dynamic Response

$V_{IN}=48V, V_{OUT}=5.0V, I_{OUT}=0.05A$ to $0.5A$,
Frequency=100Hz, Duty=50%, $C_{IN}=100\mu F, C_{OUT}=270\mu F$
CH1= V_{IN} , CH2= V_{SW} , CH3= V_{OUT} , CH4= I_{OUT}



Operational Description

The AS2461 is a high efficiency, monolithic, synchronous step-down DC/DC converter utilizing a jitter frequency, average current mode control architecture. Average current mode control enables fast and precise control of the output current. It operates through a wide VIN range and regulates with low quiescent current. An error amplifier compares the output voltage with an internal reference voltage of 1.0V and adjusts the peak inductor current accordingly. Overvoltage and undervoltage comparators will turn off the regulator.

Main Control Loop

During normal operation, the internal top power switch (N-channel MOSFET) is turned on at the beginning of each clock cycle, causing the inductor current to increase. The sensed inductor current is then delivered to the average current amplifier, whose output is compared with a saw-tooth ramp. When the voltage exceeds the Vduty voltage, the PWM comparator trips and turns off the top power MOSFET. After the top power MOSFET turns off, the synchronous power switch (N-channel MOSFET) turns on, causing the inductor current to decrease. The bottom switch stays on until the beginning of the next clock cycle, unless the reverse current limit is reached and the reverse current comparator trips. In closed-loop operation, the average current amplifier creates an average current loop that forces the average sensed current signal to be equal to the internal ITH voltage. Note that the DC gain and compensation of this average current loop is automatically adjusted to maintain an optimum current-loop response. The error amplifier adjusts the ITH voltage by comparing the divided-down output voltage (VFB) with a 1.0V reference voltage. If the load current changes, the error amplifier adjusts the average inductor current as needed to keep the output voltage in regulation.

Low Current Operation

The discontinuous-conduction modes (DCMs) are available to control the operation of the AS2461 at low currents. Burst Mode operation automatically switches from continuous operation to the Burst Mode operation when the load current is low.

Applications Information

Input Capacitor (C_{IN}) Selection

The input capacitance C_{IN} is needed to filter the square wave current at the drain of the top power MOSFET. To prevent large voltage transients from occurring, a low ESR input capacitor sized for the maximum RMS current should be used. The maximum RMS current is given by:

$$I_{RMS} \cong I_{OUT(MAX)} \frac{V_{OUT}}{V_{IN}} \sqrt{\frac{V_{IN}}{V_{OUT}} - 1}$$

This formula has a maximum at V_{IN} = 2V_{OUT}, where: I_{RMS} ≅ I_{OUT}/2.

This simple worst-case condition is commonly used for design because even significant deviations do not offer much relief. Note that ripple current ratings from capacitor manufacturers are often based on only 2000 hours of life which makes it advisable to further derate the capacitor, or choose a capacitor rated at a higher temperature than required. Several capacitors may also be paralleled to meet size or height requirements in the design. For low input voltage applications, sufficient bulk input capacitance is

needed to minimize transient effects during output load changes.

Output Capacitor (C_{OUT}) Selection

The selection of C_{OUT} is determined by the effective series resistance (ESR) that is required to minimize voltage ripple and load step transients as well as the amount of bulk capacitance that is necessary to ensure that the control loop is stable. Loop stability can be checked by viewing the load transient response. The output ripple, ΔV_{OUT} , is determined by:

$$\Delta V_{OUT} < \Delta I_L \left(\frac{1}{8 \times f \times C_{OUT}} + ESR \right)$$

The output ripple is highest at maximum input voltage since ΔI_L increases with input voltage. Multiple capacitors placed in parallel may be needed to meet the ESR and RMS current handling requirements. Dry tantalum, special polymer, aluminum electrolytic, and ceramic capacitors are all available in surface mount packages. Special polymer capacitors are very low ESR but have lower capacitance density than other types. Tantalum capacitors have the highest capacitance density but it is important to only use types that have been surge tested for use in switching power supplies. Aluminum electrolytic capacitors have significantly higher ESR, but can be used in cost-sensitive applications provided that consideration is given to ripple current ratings and long-term reliability. Ceramic capacitors have excellent low ESR characteristics and small footprints.

Inductor Selection

Given the desired input and output voltages, the inductor value and operating frequency determine the ripple current:

$$\Delta I_L = \frac{V_{OUT}}{F \times L} \left(1 - \frac{V_{OUT}}{V_{IN(MAX)}} \right)$$

Lower ripple current reduces power losses in the inductor, ESR losses in the output capacitors and output voltage ripple. Highest efficiency operation is obtained at low frequency with small ripple current. However, achieving this requires a large inductor. There is a trade-off between component size, efficiency and operating frequency. A reasonable starting point is to choose a ripple current that is about 40% of $I_{OUT(MAX)}$. To guarantee that ripple current does not exceed a specified maximum, the inductance should be chosen according to:

$$L = \frac{V_{OUT}}{F \times \Delta I_{L(MAX)}} \left(1 - \frac{V_{OUT}}{V_{IN(MAX)}} \right)$$

Once the value for L is known, the type of inductor must be selected. Actual core loss is independent of core size for a fixed inductor value, but is very dependent on the inductance selected. As the inductance or frequency increases, core losses decrease. Unfortunately, increased inductance requires more turns of wire and therefore copper losses will increase. Copper losses also increase as frequency increases. Ferrite designs have very low core losses and are preferred at high switching frequencies, so design goals can concentrate on copper loss and preventing saturation. Ferrite core material saturates "hard", which means that inductance collapses abruptly when the peak design current is exceeded. This results in an abrupt increase in inductor ripple current and consequent output voltage ripple. Do not allow the core to saturate!

Different core materials and shapes will change the size/current and price/current relationship of an inductor. Toroid or shielded pot cores in ferrite or permalloy materials are small and don't radiate much energy, but generally cost more than powdered iron core inductors with similar characteristics. The choice of which style inductor to use mainly depends on the price versus size requirements and any radiated field/EMI requirements. New designs for surface mount inductors are available from Coilcraft, Toko, Vishay, NEC/Tokin, TDK and Würth Elektronik.

Efficiency Considerations

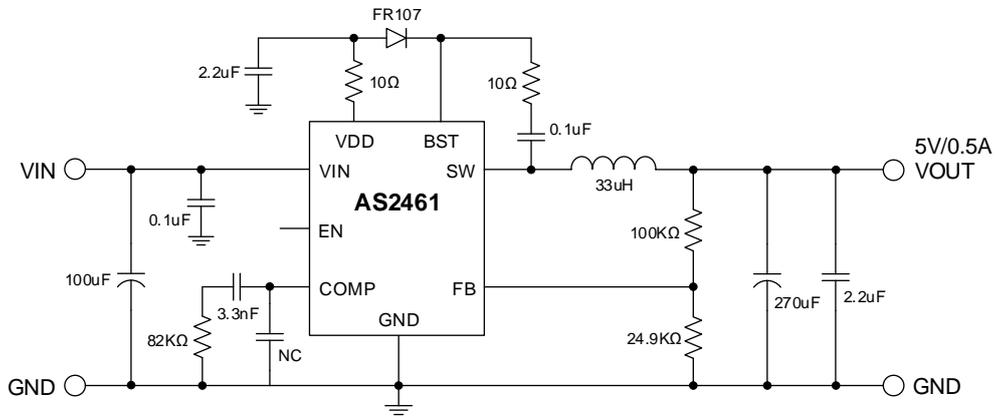
The percent efficiency of a switching regulator is equal to the output power divided by the input power times 100%. It is often useful to analyze individual losses to determine what is limiting the efficiency and which change would produce the most improvement. Percent efficiency can be expressed as: % Efficiency = 100% – (Loss1 + Loss2 + ...) where Loss1, Loss2, etc. are the individual losses as a percentage of input power. Although all dissipative elements in the circuit produce losses, three main sources usually account for most of the losses in AS2461 circuits: 1) I²R losses, 2) switching and biasing losses, 3) other losses.

Thermal Conditions

In a majority of applications, the AS2461 does not dissipate much heat due to its high efficiency and low thermal resistance. However, in applications where the AS2461 is running at high ambient temperature, high VIN, and maximum output current load, the heat dissipated may exceed the maximum junction temperature of the part.

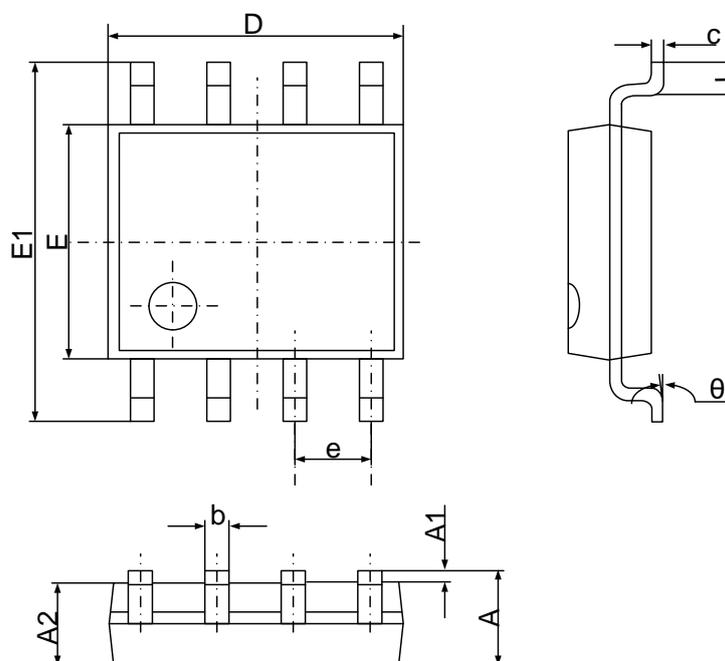
If the junction temperature reaches approximately 155°C, both power switches will be turned off until the temperature drops about 30°C cooler. To avoid the AS2461 from exceeding the maximum junction temperature, the user will need to do some thermal analysis. The goal of the thermal analysis is to determine whether the power dissipated exceeds the maximum junction temperature of the part. If the application calls for a higher ambient temperature and/or higher switching frequency, care should be taken to reduce the temperature rise of the part by using a heat sink or forced air flow.

Typical Applications



Package Description

SOP-8



符号	尺寸 (毫米)		尺寸 (英寸)	
	最小	最大	最小	最大
A	1.350	1.750	0.053	0.069
A1	0.100	0.250	0.004	0.010
A2	1.300	1.500	0.051	0.059
b	0.330	0.510	0.013	0.020
c	0.170	0.250	0.007	0.010
D	4.700	5.100	0.185	0.201
E	3.800	4.000	0.150	0.157
E1	5.800	6.200	0.228	0.244
e	1.270 (中心到中心)		0.050 (中心到中心)	
L	0.400	1.270	0.016	0.050
θ	0°	8°	0°	8°